

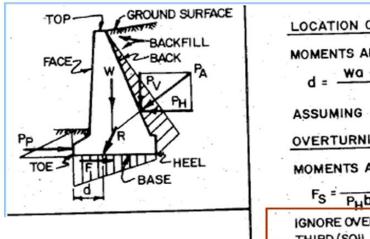








How to check retaining wall overturning stability?



LOCATION OF RESULTANT

MOMENTS ABOUT TOE: $d = \frac{wa + P_{\psi}e - P_{H}b}{w + P_{\psi}}$ ASSUMING $P_{P} = 0$ OVERTURNING

MOMENTS ABOUT TOE: $F_{S} = \frac{w_{G}}{P_{H}b - P_{\psi}e} \stackrel{>}{=} 1.5$ IGNORE OVERTURNING IF R IS WITHIN MIDDLE THIRD (SOIL), MIDDLE HALF (ROCK).

NAVFAC DM 7.2 Figure 15

Method #1

Service Load Allowable Stress Design (ASD) FS = Resisting Moment / Overturning Moment (M_r/M_o)

Method #2 (Recommended for ASD)

Ignore M_r/M_o , if the resultant falls within middle one-third (soil) or middle one-half (rock)







Method #3 2007 AASHTO LRFD, Factored (Strength Limit State), resultant should fall within middle one-half (soil) or middle three-fourths (rock)

Method #4 (Recommended for LRFD)
2012/2014/2020 AASHTO LRFD, Factored (Strength Limit State), resultant should fall within middle two-thirds (soil) or middle nine-tenths (rock)

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Question

Why "<u>middle one-half</u>" & "<u>middle two-third</u>; different from "<u>middle one-third</u>"?







2007 AASHTO LRFD

C11.6.3.3

The specified criteria for the location of the resultant, coupled with investigation of the bearing pressure, replaces the investigation of the ratio of stabilizing moment to overturning moment. Location of the resultant within the middle one-half of the base width for foundations on soil is based on the use of plastic bearing pressure distribution for the limit state.

C11.6.3.3

The specified criteria for the location of the resultant, coupled with investigation of the bearing pressure, replace the investigation of the ratio of stabilizing moment to overturning moment. Location of the resultant within the middle two-thirds of the base width for foundations on soil is based on the use of plastic bearing pressure distribution for the limit state.

2012/2014/2020 AASHTO LRFD

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However, based on personal communication with AASHTO personnel, reference of such "plastic bearing pressure distribution" was not identified...



C10.6.3.3



A comprehensive parametric study was conducted for cantilevered retaining walls of various heights and soil conditions. The base widths obtained using the LRFD load factors and eccentricity of B/4 were comparable to those of ASD with an eccentricity of B/6.

2007 AASHTO LRFD



C10.6.3.3

A comprehensive parametric study was conducted for cantilevered retaining walls of various heights and soil

conditions. The base widths obtained using the LRFD load factors and eccentricity of B/3 were comparable to those of ASD with an eccentricity of B/6. For foundations on rock, to obtain equivalence with ASD specifications, a maximum eccentricity of B/2 would be needed for LRFD. However, a slightly smaller maximum eccentricity has been specified to account for the potential unknown future loading that could push the resultant outside the footing dimensions.

2012/2014/2020 AASHTO LRFD

Cautions

Do Not Mix Up the Use of Criteria between ASD and LRFD Designs







Case Studies: Isolated Bridge Abutment and Bridge Foundation

Geotechnical and Structural Design Considerations



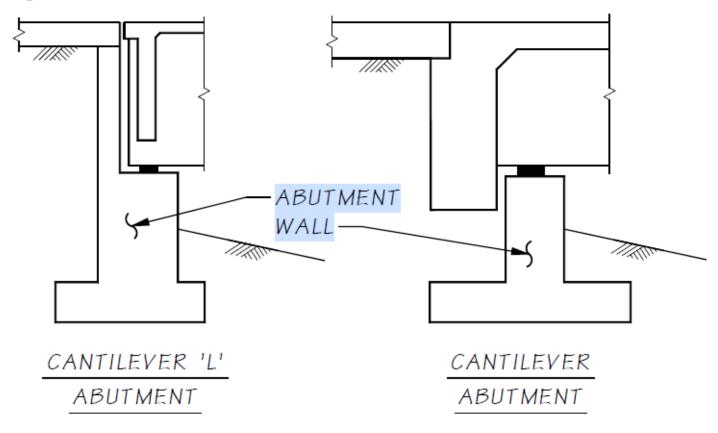




Conventional Cast-in-Place (CIP) Reinforced Concrete Abutment Wall

WSDOT Bridge Design Manual M 23-50.19 July 2019

Figure 7.5.1-2 Cantilever Abutments









Mechanical Stabilized Earth (MSE) Wall



Publication No. FHWA-NHI-10-024 FHWA GEC 011 – Volume I November 2009

NHI Courses No. 132042 and 132043

Design and Construction of Mechanically Stabilized Earth Walls and Reinforced Soil Slopes – Volume I

and

Developed following:

AASHTO LRFD Bridge Design Specifications, 4th Edition, 2007, with 2008 and 2009 Interims.

AASHTO Specificat

AASHTO LRFD Bridge Construction Specifications, 2nd Edition, 2004, with 2006, 2007, 2008, and 2009 Interims.







<u>Pile/Drilled Shaft Supported Bridge Foundation</u> <u>Behind MSE Abutment Walls</u>







Photo from WSP (Previous AMEC) Project 2013

Photo from Khodair and Hassiotis, 2005

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Soil Nail



U.S. Department of Transportation Federal Highway Administration Publication No. FHWA-NHI-14-007 FHWA GEC 007 February 2015

NHI Course No. 132085

Shored Mechanically Stabilized Earth (SMSE) Wall Systems Design Guidelines

Shored MSE

(SMSE) Walls

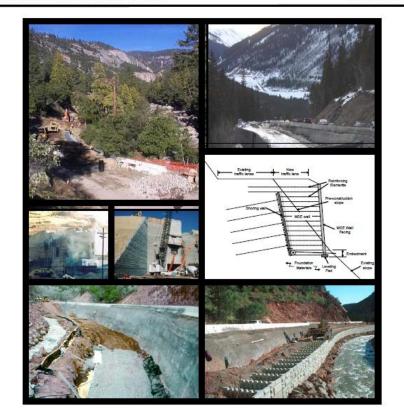
Publication No. FHWA-CFL/TD-06-001

February 2006

Soil Nail Walls Reference Manual

Developed following: AASHTO LRFD Bridge Design Specifications, 7th Edition.







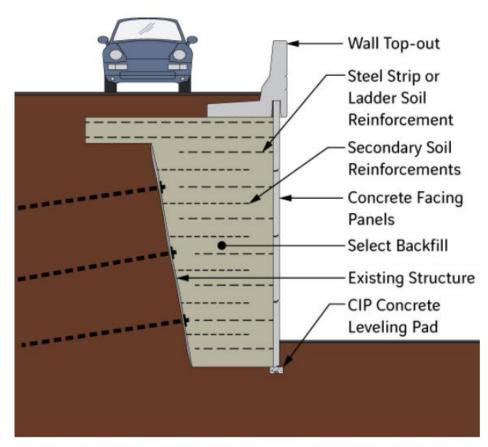


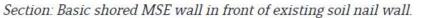


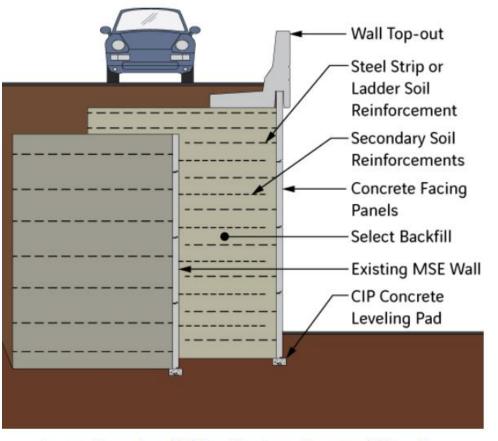
Shored MSE (SMSE) Walls Cut / Fill / Widening

Shored Reinforced Earth® MSE Retaining Walls

(From: https://reinforcedearth.com/products/retaining-walls/special-design/)







11.







Bridge Abutment Walls (Underpass Widening)

"Combo" - Cut Soil Nail Wall/Soldier Pile & Lagging / Anchor Tiebacks/Mechanical Plate Anchors /Precast Panel Facia w/ Flowable Fill



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> FDOT I-10 Scenic Hwy Project (Schnabel Engineering Project, 2006)







Geosynthetic Reinforced Soil (GRS) Wall

In Memory of <u>Prof. Jonathan T.H. Wu (1951 - 2020)</u>
University of Colorado Denver
Director of Reinforced Soil Research Center

Chou, N.N.S., <u>Ww. J.T.M.</u>: Investigating Performance of Geosynthetic-Reinforced Soil Walls, report no. CDOT-DTD-93-21, Colorado Department

of Transportation <u>[[1993]</u>

GRS Abutments

Combination of gravel and closely spaced layers of geotextile or geogrid; commonly w/o utilizing an approach slab

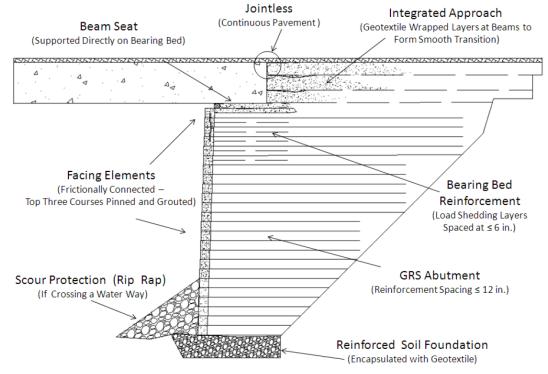


Figure 1. Illustration. Typical GRS-IBS cross section.

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Geosynthetic Reinforced Soil (GRS) Wall

Geosynthetic Reinforced Soil Integrated Bridge System Interim Implementation Guide

PUBLICATION NO. FHWA-HRT-11-026

JUNE 2012

Integrated Bridge System (GRS-IBS); GRS Abutments
Cost effective; esp. for bridge supported on shallow
foundations



How to <u>reduce</u> lateral earth pressures acting on bridge abutment walls?

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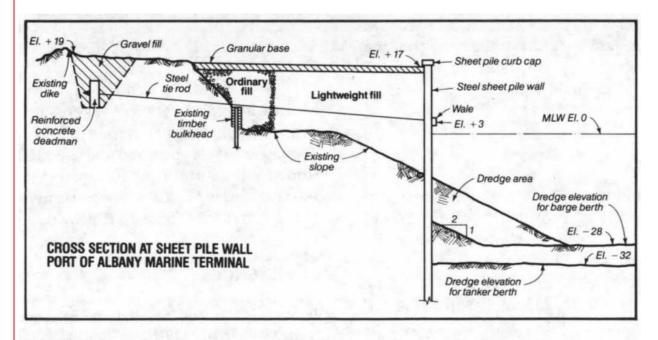






Retaining Walls with Lightweight Fill (Lightweight Fill/Aggregate, Geofoam, etc.)





GEOFOAM

Granular Drain

Pipe

Soil Cover or Pavement

Retaining Wall or Abutment

Drain
Pipe

FIGURE 6 Rehabilitation of port of Albany, N.Y., marine terminal.

Figure 2.3. Typical Construction Detail for EPS GeoFoam Backfilled Earth Retention Structure (from Negussey 1997)



Retaining Walls with Shredded Tire Fill





GUIDELINES FOR PROJECT SELECTION, DESIGN, AND CONSTRUCTION OF TIRE SHREDS IN EMBANKMENTS



GEOTECHNICAL ENGINEERING MANUAL GEM-20 Revision #2

GEOTECHNICAL ENGINEERING BUREAU

JULY 2008



FINAL REPORT

FIELD STUDY OF A SHREDDED-TIRE EMBANKMENT IN VIRGINIA

Edward J. Hoppe, Ph.D., P.E. Senior Research Scientist Virginia Transportation Research Council

> W. Grigg Mullen, Ph.D., P.E. Professor Virginia Military Institute

> > April 2004 VTRC 04-R20

SSRG International Journal of Civil Engineering (SSRG - IJCE) - Volume 5 Issue 12 - December 2018

Reduction of Dynamic Earth Pressure on Retaining Wall Backfilled with STC: A Review

¹Samreen Bano, ²Dr. Sabih Ahmad

¹M.tech Student, Department of Civil Engineering, Integral University, Lucknow, Uttar Pradesh, 226026,India.

²Associate professor, Department of Civil Engineering, Integral University, Lucknow, Uttar Pradesh, 226026,India.



How to <u>relieve (eliminate)</u> lateral earth pressures acting on bridge abutment walls?

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Reinforced Earth Structures to Relieve Walls of Earth Pressure (Raithel, et al. 2012)

(https://www.kup-geotechnik.com/media/140625_10icg_earthpressure.pdf)

"... reduce the earth pressure ... wrap back geotextile reinforced earth structures (GRE). earth pressure can be reduced to zero, <u>leaving a gap (4 to 20 inches)</u> in between wall and GRE. horizontal (wall) deformations ...maximum around 2 cm for the 10 m

high GRE (0.2%H)...."





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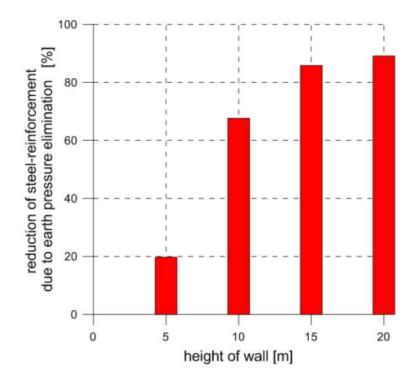




Reinforced Earth Structures to Relieve Walls of Earth Pressure (Raithel, et al. 2012)

(https://www.kup-geotechnik.com/media/140625_10icg_earthpressure.pdf)

Cost-Effectiveness Reduction of steel-reinforcement >60% for wall heights >30 feet



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NCHRP Project 20-68D, Scan 19-01

Leading Practices for Detailing Bridge Ends and Approach Pavements To Limit Distress and Deterioration

Supported by the

National Cooperative Highway Research Program

PREPARED BY

Jason DeRuyver, P.E. Michigan DOT, Chair

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Jill Walsh, Ph.D., P.E. Saint Martin's University, Subject Matter Expert

Devan Eaton, P.E. Maine DOT

Bijan Khaleghi, Ph.D., P.E., S.E. Washington State DOT

Adam Lancaster, P.E. Louisiana DOTD





SCAN MANAGEMENT

Arora and Associates, P.C. Lawrenceville, NJ

October 2020

Soil reinforcement can be used to improve the approach embankment. Caltrans' End Bent with **Isolated MSE abutment** type is shown in **Figure 36**. **Figure 86** shows the 6 inch layer of TPB (treated permeable base) Caltrans uses under the approach slab.

WSDOT: An option to reduce seismic load from approach fill to abutment's wall is to isolate the fill with isolated abutments by providing a six-foot gap between the soil and the abutment wall. Figure 99 shows an isolated abutment with a separate retaining system to support the embankment. Figure 100 shows a similar concept but with a fascia wall to provide separation









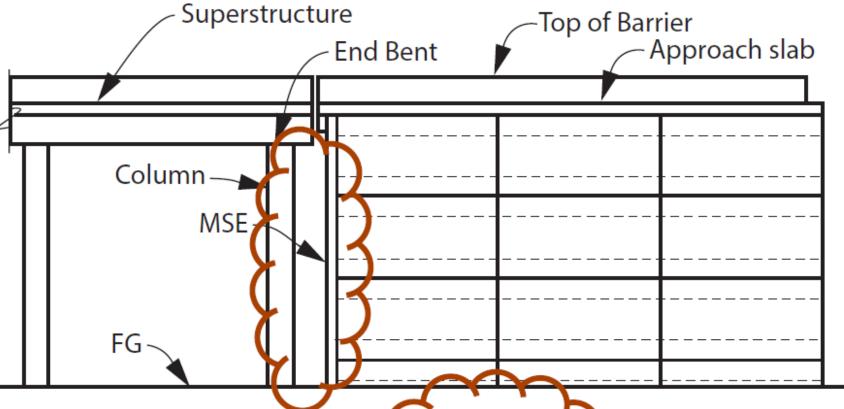


Figure 4B - End Bent with Isolated MSE on Three Sides

Figure 4 - Application of MSE at Bridge Approaches







Design Considerations for Isolated Bridge Abutment



Memo to Designers 5-1 • March 2017

"An <u>adequate gap</u> is required to accommodate bridge movements ... <u>No special design is required for either</u> the abutment or MSE ..."

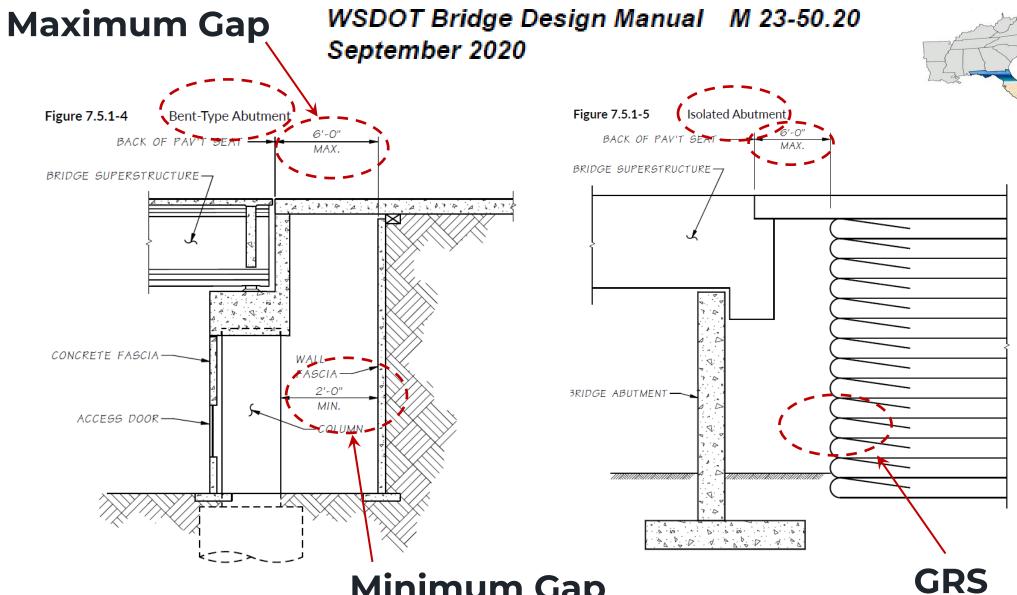
"The gap ... must be <u>wide enough</u> to avoid contact of the two isolated structures due to movements caused by earthquakes."

Question

What is the "adequate gap / wide enough"?







Minimum Gap

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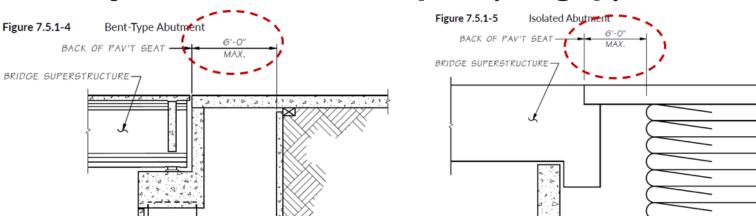




WSDOT Bridge Design Manual M 23-50.20 September 2020

"The gap ... shall not be less than 6 inches. The approach embankment wall does not require a fascia."; "The minimum gap between the back of the columns, piles, or shafts and the retained structure shall be 2'-0" to allow for inspection access."

Question Why "max. 6-ft clear span (air gap)"?





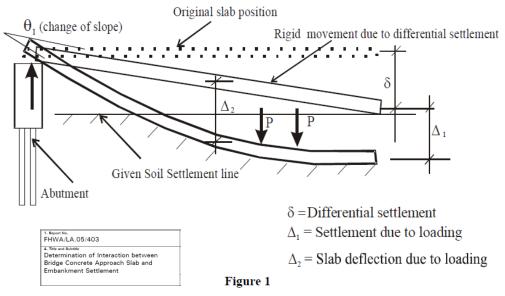




Design Considerations for Isolated Bridge Abutment

Requiring a bridge approach structural slab

- max. 6'-0" Clear Span (Air Gap)
- Optimize slab structural design; consider embankment settlements (static & post-earthquake)
- Provide inspection access



WSDOT BDM (2020)

"The approach slab shall be designed as a beam pinned at the back of pavement seat. The approach slab shall support traffic live loads and traffic barrier reactions."

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Project Case Study (1)

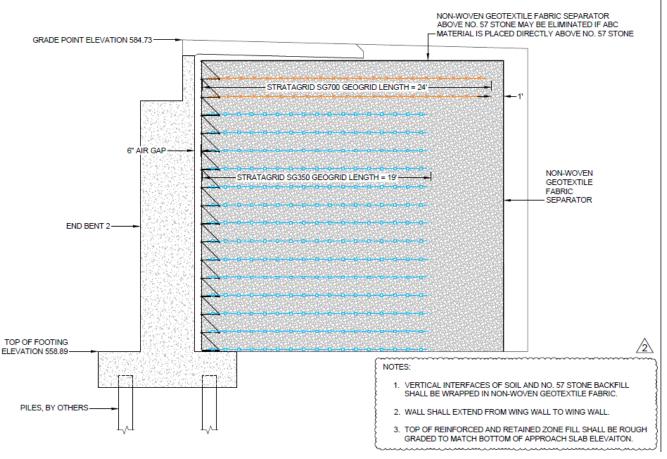
Charlotte, North Carolina USA

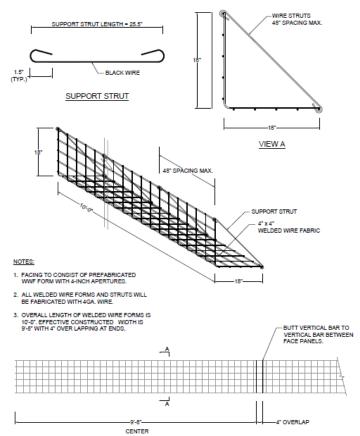




Isolated Wired Basket Facing Wall w/ 6" Air Gap













Pile-Supported Bridge Abutment Wall (Constructed First)



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Wired Basket Facing Reinforced Earth Wall (Constructed Next)



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Project Case Study (2)

Seattle, Washington USA









I-405 Bellevue to Renton Express Toll Lanes Design-Build Project

Client

Washington DOT Flatiron/Lane JV

Location

King County, Washington

Project Duration

2019-present

Contract Value

\$705 Million

WSP Role: Design Prime Team Member

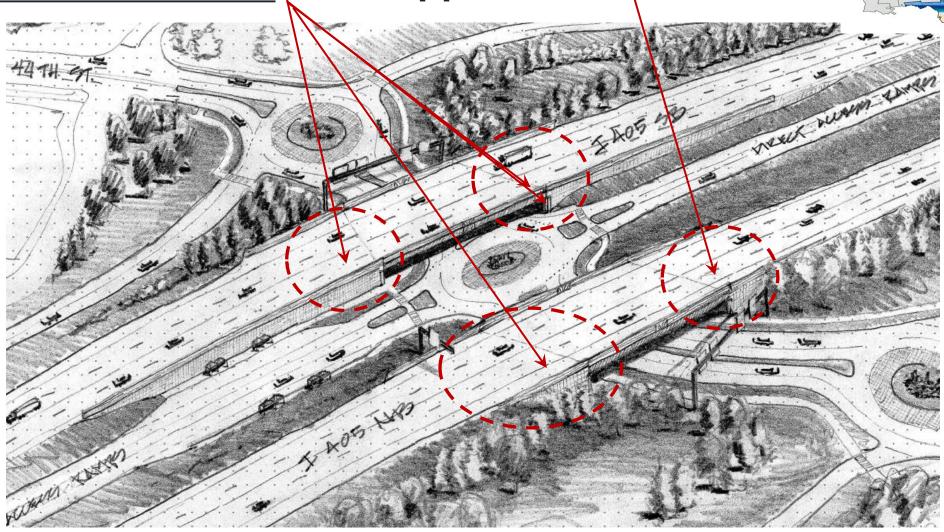
- Geotechnical/Structural/Civil/ Roadway
 Design Leads
- Environmental (Fish passage and stream restoration)

si uec 2022 Daytona Beach, Flori October 17-20, 2022



"Fill" Bridge Approach
Embankments

"Cut" Soil Nail Bridge Approach Embankment

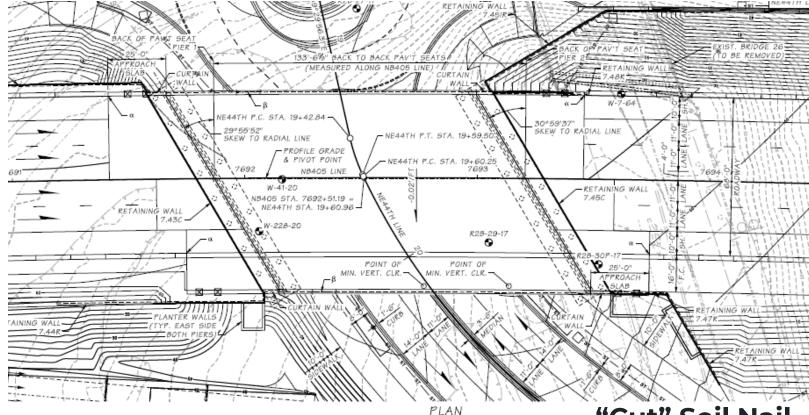


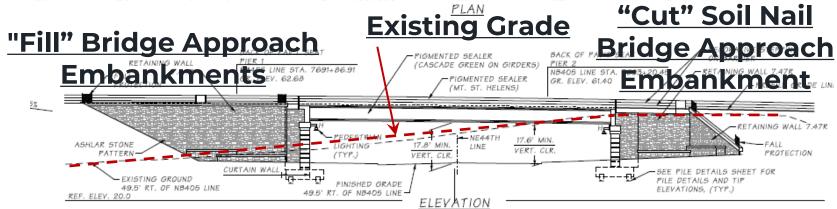
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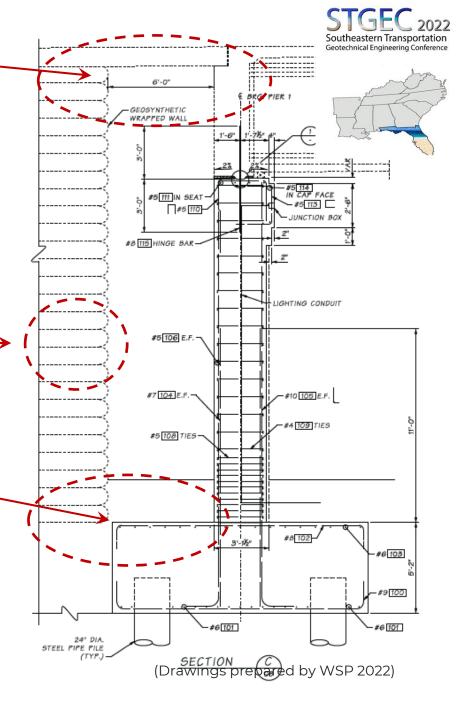
Design Air Gap 6'-0"

Consider long term(static & Postearthquake) embankment settlements; allow bridge approach slab spanning max. 17'-0" between the back of pavement seat and the bridge abutment wall.

GRS Wall / Wired
Basket Wall

Keep Embankment Footprint Outside of Bridge Abutment Wall Pile Cap

Reduce vertical loading on pile; consider lateral pressures acting on the side of pile cap due to surcharge effect.









"Cut" Bridge Approach EmbankmentSite Preparation



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"Cut" Bridge Approach Embankment Bridge Foundation Piles Installed First



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"Cut" Bridge Approach Embankment Bridge Foundation Piles Installed First







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"Cut" Bridge Approach Embankment Soil Nail Wall Constructed Next



SIGEC 2022 Daytona Beach, Flori October 17-20, 2022







"Fill" Bridge Approach Embankment Bridge Foundation Piles Installed First



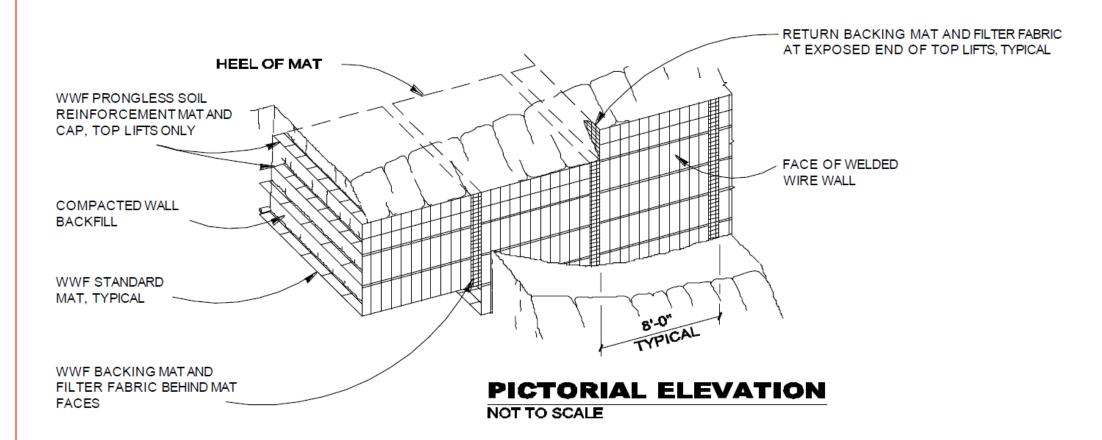
SIGEC 2022 Daytona Beach, Flori October 17-20, 2022







"Fill" Bridge Approach Embankment Wired Basket Wall Constructed Next, w/o Structural Facia





<u>Isolated Bridge Abutment and</u> <u>Bridge Foundations</u>





Pros

- Eliminate earth pressures acting on bridge abutment wall.
- Reduce compressive loading demand and potential downdrag on foundation piles; esp. for walls w/ greater heights and seismic loading.
- Do not require a fascia for the isolated embankment, though require curtain walls to hide the air gap.
- Construction time efficiency / schedule flexibility







Isolated Bridge Abutment and Bridge Foundations Cons

- Require the bridge approach slab designed as a structural element; by considering the air gap and long-term embankment settlements (static & postearthquake).
- Bridge foundation piles may require additional PDA/CAPWAP evaluation to verify design required tension/uplift resistance (subject to seismic loading).

Further Considerations

- Is a single-span bridge with isolated abutments still a single-span bridge for seismic considerations?
- Future inspection access
- Form work / Falsework for approach slab at gap

Thank you







wsp.com